

# Extraction of MOS Model 7 DC Parameters using Automation Tools

Step:

Automated Data Collection.

Computer Usage:

Accutest 3600, PDP11

Files:

input: Test Table;  
output: fn.out

Data transfer to IBM

DEC Ethernet, VMS VAX,  
IBM VM.

fn\*.out  
(many \*.out files)

Data Preview using Topex

Uses TOPEX in manual,  
local mode to draw  
device characteristic  
graphs.

Topex command  
file( \*.topex),  
Topex init file  
(\*data),  
Accutest data.

Automated TOPEX

Merge Accutest files,  
Prepare \*.list file,  
Run "TOPBAT" & "TOPRDR"

input: \*.list,  
\*.out.  
output: \*.total

Automated Geometry  
Parameter Extraction

Run "ALLMAX"

input: \*.total  
output: \*.maxise

Confirm Geometry Fit

Run "VIEWMINI"

input: \*.total,  
\*.maxiset data  
output graphs

Create the ESPICE  
parameter model file

XEDIT

input: old \*.EDOS

Model Verification

"FASTSLOW"

input: \*.EDOS,  
Accutest data

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 Subject: MOS Model 7C Equations

Date: April 13, 1987

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**Model 7C:**

- (1)  $T = T(^{\circ}C) + 273.15$
- (2)  $T_n = T_{nom}(^{\circ}C) + 273.15$
- (3)  $V_t = \frac{kT}{q}$
- (4)  $V_{t_n} = \frac{kT_n}{q}$
- (5)  $E_g(T) = 1.16 - \left( \frac{7.02 \times 10^{-4} T^2}{T + 1108.} \right)$
- (6)  $n_i(T) = n_i \cdot \left( \frac{T}{T_n} \right)^{\frac{3}{2}} \exp \left( \frac{E_g}{2V_{t_n}} - \frac{E_g(T)}{2V_t} \right)$
- (7)  $2\Phi_F = PHI \cdot \left( \frac{T}{T_n} \right) + V_t \cdot \ln \left( \frac{n_i}{n_i(T)} \right)$
- (8)  $V_{TNT} = VTN|_{V_{sb}=V_{sb_{ref}} \& T=T_n} + TCVT \cdot (T - T_n)$
- (9)  $\beta_N = BETAN \cdot \left( \frac{T_n}{T} \right)^{TBETA}$
- (10)  $\theta'_{3N} = TH3N + TTH3N \cdot (T - T_n)$
- (11)  $G\theta'_{3N} = GTH3N + TGTH3N \cdot (T - T_n)$
- (12)  $W = W_N + WTOL$
- (13)  $L = L_N + LTOL - 2 \cdot LAP$
- (14)  $K = KN + GKN \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DKN \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$
- (15)  $Ko = KON + GKON \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DKON \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$
- (16)  $V_{SBX} = V_{SBXN} + G_{V_{SBXN}} \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + D_{V_{SBXN}} \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$
- (17)  $V_{TOT} = V_{TNT} - K \cdot \left( \sqrt{V_{sb_{ref}} + 2\Phi_F} - \sqrt{2\Phi_F} \right)$
- (18)  $V_{TO} = V_{TOT} + G_{VTN} \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + D_{VTN} \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$

$$(19) \quad \theta_1 = TH1N + GTH1N \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DTH1N \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(20) \quad \theta_2 = TH2N + GTH2N \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DTH2N \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(21) \quad \theta_3 = \theta'_{3N} + G\theta'_{3N} \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DTH3N \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(22) \quad \gamma = GAMMAN + GGAMN \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) \\ + DGAMN \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(23) \quad SH = SHIFTN + GSHIFT \cdot \left( \frac{1}{L^2} - \frac{1}{L_{ref}^2} \right)$$

$$(24) \quad n = NN + GNN \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right)$$

$$(25) \quad p = PN + GPN \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right)$$

$$(26) \quad a = AVA + GAVA \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DAVA \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(27) \quad b = AVB + GAVB \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DAVB \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(28) \quad c = AVC + GAVC \cdot \left( \frac{1}{L} - \frac{1}{L_{ref}} \right) + DAVC \cdot \left( \frac{1}{W} - \frac{1}{W_{ref}} \right)$$

$$(29) \quad DELVX = 0.3$$

$$(30) \quad Kap = \sqrt{V_{sb} + 2\Phi_F} - \sqrt{2\Phi_F}$$

$$(31) \quad Kap1 = \sqrt{V_{SBX} - DELVX + 2\Phi_F} - \sqrt{2\Phi_F}$$

$$(32) \quad Kap2 = \sqrt{V_{SBX} + DELVX + 2\Phi_F} - \sqrt{2\Phi_F}$$

If ( $Kap \leq Kap1$ ) Then

$$(33) \quad V_{TS} = V_{TO} + Ko \cdot Kap$$

$$(34) \quad \delta = \frac{Ko}{2\sqrt{1 + V_{sb} + 2\Phi_F}}$$

If ( $Kap \geq Kap2$ ) Then

$$(35) \quad V_{TS} = V_{TO} + \frac{(Ko - K)(Kap1 + Kap2)}{2} + K \cdot Kap$$

$$(36) \quad \delta = \frac{K}{2\sqrt{1 + V_{sb} + 2\Phi_F}}$$

If ( $Kap1 < Kap < Kap2$ ) Then

$$(37) \quad V_{TS} = V_{TO} + Ko \cdot Kap - \frac{(Ko - K)(Kap - Kap1)^2}{2(Kap2 - Kap1)}$$

$$(38) \quad \delta = \frac{Ko - \frac{(Ko - K)(Kap - Kap1)}{(Kap2 - Kap1)}}{2\sqrt{1 + V_{sb} + 2\Phi_F}}$$

$$(39) \quad \Delta V_T = SH \cdot (1 + p \cdot V_{sb}) \cdot V_{ds}^n$$

$$(40) \quad V_T = V_{TS} - \Delta V_T$$

$$(41) \quad V_o = 0.5$$

*If*  $((V_{gs} - V_T) > 2V_o)$  *Then*

$$(42) \quad V_{GT} = V_{gs} - V_{TS} + \gamma \cdot V_{ds}$$

*If*  $((V_{gs} - V_T) \leq 2V_o)$  *and*

$((V_{gs} - V_T) \geq 0)$  *Then*

$$(43) \quad V_{GT} = V_{gs} - V_T + \frac{(\gamma \cdot V_{ds} - \Delta V_T)}{2V_o} \cdot (V_{gs} - V_T)$$

*If*  $((V_{gs} - V_T) < 0)$  *Then*

$$(44) \quad V_{GT} = V_{gs} - V_T$$

$$(45) \quad SUBTHN = 2 \cdot M$$

$$(46) \quad V_{ON} = SUBTHN \cdot V_t$$

$$(47) \quad V_{GT_{orig}} = V_{GT}$$

*If*  $(V_{GT} \leq V_{ON})$  *Then*

$$(48) \quad V_{GT} = V_{ON}$$

*If*  $(\theta_3 \leq 1 \times 10^{-6})$  *Then*

$$(49) \quad \theta_3 = 1 \times 10^{-6}$$

$$(50) \quad V_{DSS} = \left( \frac{1}{\theta_3} \right) \cdot \left( \sqrt{1 + \frac{2\theta_3 V_{GT}}{(1+\delta)}} - 1 \right)$$

$$(51) \quad V_r = V_{DSS}$$

*If*  $(V_{ds} < V_{DSS})$  *Then*

$$(52) \quad V_r = V_{ds}$$

$$(53) \quad I_d = \beta_N \frac{W}{L} \cdot \frac{(V_{GT} - \frac{(1+\delta)}{2} \cdot V_r) \cdot V_r}{(1 + \theta_1 \cdot (V_{gs} - V_{TS}) + \theta_2 \sqrt{V_{sb} + 2\Phi_F}) \cdot (1 + \theta_3 \cdot V_r)}$$

*If*  $(V_{GT_{orig}} \leq V_{ON})$  *Then*

$$(54) \quad I_d = I_d \cdot \exp\left(\frac{V_{GT_{orig}} - V_{ON}}{M \cdot V_t}\right)$$

$$(55) \quad V_{EM} = c \cdot V_{DSS}$$

$$(56) \quad I_b = 0$$

*If*  $(V_{ds} > V_{EM})$  *Then*

$$(57) \quad I_b = I_d \cdot a \cdot \exp\left(\frac{-b}{V_{ds} - V_{EM}}\right)$$

$$(58) \quad I_d = I_d + I_b$$